

# E UestraserLVL 

LVL User's Guide Technical Data for LVL Headers, Beams, Column Applications for Residential Floor and Roof Systems


## Quality Products - Committed Service

## OUR HISTORY

In 1955, three Ketcham brothers, Henry Jr., William, and Samuel, started West Fraser by acquiring a small lumber planing mill in Quesnel, BC. Throughout the years, they continued to make various sawmill acquisitions in the interior of British Columbia, which included the associated timber rights. In 1979, West Fraser entered the pulp industry, constructing a joint venture mill in Quesnel. West Fraser's expansion continued into Alberta in 1989 when they entered into a joint venture newsprint mill in Whitecourt. the Company's growth continued in Alberta with the acquisition of a sawmill, MDF plant, and pulp mill in 1995 and a plywood mill, stud mill and veneer mill in 1999. In 2000, West Fraser entered the United States by

## OUR ENVIRONMENTAL STEWARDSHIP

West Fraser Timber Co. Ltd. is committed to responsible stewardship of the environment. A philosophy of continual improvement of our forest practices and manufacturing procedures has been adopted to optimize the use of resources and minimize or eliminate the impact of our operations on the environment.

West Fraser recognizes that environmental excellence is an integral aspect of long-term business success. Our Company and its employees are committed to the following:

- Complying with all applicable environmental laws and regulations, and with other requirements to which the organization subscribes.
acquiring two sawmills in the U.S. south. A major acquisition occurred in 2005 with the purchase of Weldwood of Canada. With this purchase, West Fraser entered the engineered wood business by acquiring the world's first continuous laminated veneer lumber press.

West Fraser expanded further in 2007 when the Company acquired 13 additional sawmills in the southern U.S. from International Paper Co. This added 1.8 billion board feet of lumber capacity to West Fraser for a total capacity of more than 6 billion board feet, making West Fraser one of the largest lumber producers in North America.

- Preventing pollution and continuing to improve our environmental performance by setting and reviewing environmental objectives and targets.
- Conducting periodic environmental audits.
- Providing training for employees and contractors to ensure environmentally responsible work practices.
- Communicating our environmental performance to employees, customers, shareholders, local communities and other stakeholders.
- Reviewing, on a regular basis, this policy to ensure that it reflects the Company's ongoing commitment to environmental stewardship.


## OUR VISION

West Fraser's vision is to be the leading forest products company in Canada. Our goals are simple - leadership in profits, responsibility in communities, excellence in people and strength in products.

## A Word About LVL Grades

## DID YOU KNOW THAT .. .

If you are using 2.0 E beams and headers exclusively in residential wood construction, you are leaving money on the table approximately $85 \%$ of the time.

When sizing beams and headers, you need to have sufficient moment capacity ( $\mathrm{F}_{\mathrm{b}}$ ), sufficient shear capacity $\left(\mathrm{F}_{\mathrm{v}}\right)$, sufficient stiffness (EI) to satisfy the live and total load deflection criteria and you need to have adequate bearing sizes ( $\mathrm{F}_{\mathrm{C}_{\perp}}$ ).

The industry markets LVL beams and headers based on the MOE value (modulus of elasticity $=\mathrm{E}$ ) which along with the size of the beam (moment of inertia $=1$ ) determines the stiffness (EI) of the beam. The stiffness of a beam determines how much deflection a beam will experience under a given load. Deflection is a performance criteria established by

building codes (L/360). Stiffness is not the same as strength!
Not all applications are controlled by stiffness, many are controlled by strength ( $F_{\mathrm{b}}$ and $\mathrm{F}_{\mathrm{v}}$ ). In some applications, a 1.9E or 2.0 E beam cannot be used as a substitute for a 1.8 E beam that has superior strength properties ( $\mathrm{F}_{\mathrm{b}}$ and $\mathrm{F}_{\mathrm{v}}$ ).

A beam $16^{\prime}$ long, carrying 300 PLF , with 1.9 E material will deflect 0.0344 inches less $\left(1 / 32^{\prime \prime}\right)$ under total load compared to the same beam with 1.8 E material. This is not much, especially when you consider the premium you pay for high MOE


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## PRODUCT LINE



With the use of ultrasonic grading technology, West Fraser wisely utilizes the inherent attributes of its wood resources to manufacture products that effectively satisfy the needs of the market while at the same time, contribute to a greener, more sustainable environment. In addition, these attributes also allow for superior fiber bending strength and workability.

## West Fraser ${ }^{\text {TM }}$ LVL $3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E}$

- $13 / 4^{\prime \prime}$ and $31 / 2^{\prime \prime}$ thick in

I-Joist and lumber compatible depths to 24 " deep

West Fraser ${ }^{\text {TM }}$ LVL $3000 F_{b}-1.9 \mathrm{E}$

- $13 / 4^{\prime \prime}$ thick in I-Joist and lumber compatible depths to $24^{\prime \prime}$ deep

West Fraser ${ }^{\text {TM }}$ LVL $3000 F_{b}-1.8 \mathrm{E}$

- $11 / 2^{\prime \prime}, 13 / 4^{\prime \prime}$, and $3^{1 / 2 "}$ " thick in I-Joist and lumber compatible depths to $18^{\prime \prime}$. ( $13 / 4^{\prime \prime}$ and $31 / 2^{\prime \prime}$ to $24^{\prime \prime}$ ), $3^{1 ⁄ 2}{ }^{\prime \prime}$ thick in columns

West Fraser ${ }^{\text {TM }}$ LVL $2750 F_{b}-1.7 E$

- $13 / 4^{\prime \prime}$ and $31 / 2^{\prime \prime}$ thick in I-Joist and lumber compatible depths to $24^{\prime \prime}$ deep

All products have face, back and edges sealed for improved performance under normal construction exposure
CODE EVALUATION REPORT NUMBERS: CCMC 12904-R
Check product availability with supplier prior to specifying LVL sizes.

## STORAGE, HANDLING AND INSTALLATION

Failure to follow good procedures for installation, storage and handling could result in unsatisfactory performance and unsafe structures.

- West Fraser ${ }^{\text {TM }}$ LVL should be stored lying flat and protected from the weather.
- Stickers to be aligned one above the other and spaced no more than 8'-0" apart.
- Do not exceed a storage bundle height of $10^{\prime}-0$ " .
- Keep the material above ground to minimize the absorption of ground moisture and allow circulation of air.
- Report all forklift damage prior to shipment.
- West Fraser ${ }^{\text {TM }}$ LVL is for use in covered, dry conditions only. Protect from the weather on the job site both before and after installation.
- Except for cutting to length, West Fraser ${ }^{\text {rM }}$ LVL shall not be cut, drilled or notched. Heel cuts may be possible. Contact your West Fraser representative.
- Place first set of stickers on hard, level dry surface.
- Do not install any damaged LVL.

CAUTION: Wrap may be slippery when wet


These are general recommendations and in some cases, additional precautions may be required.


## DESIGN PROPERTIES

$3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E} 13 / 4^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51⁄2" | 71/4" | 91/4" | 91/2" | 111/2" | 117/8" | 14" | 16" | 18" | 24" |
| Moment (ft.lbs.) | 4134 | 6967 | 11037 | 11608 | 16652 | 17693 | 24146 | 31073 | 38816 | 66835 |
| Shear (Ibs.) | 3199 | 4217 | 5381 | 5526 | 6690 | 6908 | 8144 | 9307 | 10471 | 13961 |
| Moment of Inertia (in^4) | 24 | 56 | 115 | 125 | 222 | 244 | 400 | 597 | 851 | 2016 |
| Weight (lbs./lin.ft.) | 2.7 | 3.6 | 4.6 | 4.7 | 5.7 | 5.9 | 7.0 | 8.0 | 9.0 | 12.0 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime}$ o/c or closer.
2. Lateral support of beam is required at bearing locations.
3. All $16^{\prime \prime}$ and greater beam depths are to be used in multiple member units only.
$3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E} 312^{\prime \prime}$ " WEST FRASER ${ }^{\text {TM }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 7114" | 91/4" | 91/2" | 111/2" | 117/8" | 14" | 16" | 18" | 24" |
| Moment (ft.lbs.) | 8269 | 13933 | 22075 | 23215 | 33305 | 35386 | 48292 | 62146 | 77631 | 133669 |
| Shear (Ibs.) | 6398 | 8434 | 10762 | 11052 | 13380 | 13816 | 16288 | 18614 | 20942 | 27922 |
| Moment of Inertia (in^4) | 49 | 111 | 231 | 250 | 444 | 488 | 800 | 1195 | 1701 | 4032 |
| Weight (lbs./lin.ft.) | 5.5 | 7.2 | 9.2 | 9.5 | 11.5 | 11.8 | 14.0 | 15.9 | 17.9 | 23.9 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. Lateral support of beam is required at bearing locations.
$3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E} 13 / 4^{\prime \prime}$ AND $31 / 2^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL AVAILABLE SIZES

$3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E}$ WEST FRASER ${ }^{T M}$ LVL SPECIFIED STRENGTHS (STANDARD TERM)

[^0]\[

$$
\begin{aligned}
\mathrm{E} & =2.0 \times 10 \wedge 6 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{b}} & =5729 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{V}} & =554 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { perp })} & =1300 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { para })} & =4786 \mathrm{psi}
\end{aligned}
$$
\]

1. $\mathrm{F}_{\mathrm{b}}$ based on $12^{\prime \prime}$ depths. For other depths, multiply by $(12 / \mathrm{d}) \wedge(1 / 9)$.

## GENERAL NOTES

- Tables are for one-ply $13 / 4^{\prime \prime}$ beams. When properly connected, double the values for two-ply beams, triple for three. Minimum bearing lengths shown for one-ply will be the same for two-ply and three-ply. See page 9 for multiple-ply connection details.
- Resistances shown are the maximum factored and/or unfactored resistances, in pounds per lineal foot, that can be applied to the beam in addition to its own weight.
- Tables are based on uniform loads and the most restrictive of simple or continuous spans and dry-use conditions. Refer to West Fraser's sizing software for other loads or span configurations.
- Lateral support of beam compression edges is required at intervals of $24^{\prime \prime}$ o/c or closer.
- Lateral support of beams is required at bearing locations.
- Spans of multiple spans must be at least $40 \%$ of adjacent span.
- West Fraser ${ }^{\text {rM }}$ LVL beams are made without camber; therefore, in addition to complying with the deflection limits of the applicable building code, other deflection considerations, such as long term deflection under sustained loads (including creep), must be evaluated.
- All $16^{\prime \prime}$ and deeper beams are to be used in multiple member units only.
- Unfactored total load resistance is limited to a deflection of $\mathrm{L} / 240$. Unfactored live load resistance is based on a deflection of L/360. Check local code requirements for other deflection criteria.
- For an unfactored live load deflection limit of L/480, multiply UNFACTORED LOAD L/360 resistance by 0.75 . The resulting unfactored live load shall not exceed the total factored load shown.
- Roof must have positive slope in order to prevent ponding.
- Tables will accommodate beam slopes to a maximum of 2:12.
- Bearing lengths are based on 1300 psi specified strength for $3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E}$ Grade materials which cannot be increased for duration of load. Bearing length may need to be increased if support member's allowable bearing stress is less.
- Spans shown are measured centre-to-centre of bearing.


## INSTRUCTIONS FOR USE

1. Determine the factored total load and unfactored total and live load on the beam in pounds per lineal foot (plf).
2. Locate a span that meets or exceeds the required beam span, centre-to-centre of bearing.
3. Scan from left to right within the SPAN row until you find a cell where; (1) the UNFACTORED LOAD L/360 resistance meets or exceeds the unfactored live load, (2) the UNFACTORED LOAD L/240 resistance
meets or exceeds the unfactored total load and (3) the FACTORED TOTAL LOAD resistance meets or exceeds the factored total load. All three rows must be checked and satisfied. Where no unfactored resistances are shown, factored total load will control.
4. To size a member for a span not shown, use capacities for the next larger span shown.

FACTORED RESISTANCE TABLE (pounos perlineal foot)

## $3100 \mathrm{~F}_{\mathrm{b}}$-2.0E West Fraser" ${ }^{\text {mim }}$ LVL - FLOOR or Roof (Standard Term)

| Span (ft) |  | 13/4" WIDTH |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Depth | 5-1/2" | 7-1/4" | 9-1/4" | 9-1/2" | 11-1/2" | 11-7/8" | $14{ }^{\prime \prime}$ | 16" | 18" | 24" |
| 6 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) | 305 455 916 $1.5 / 3.8$ | 660 986 1337 $2.5 / 6.4$ | $\begin{gathered} 1263 \\ 1802 \\ 3.5 / 8.7 \end{gathered}$ | $\begin{gathered} 1353 \\ 1863 \\ 3.6 / 9.0 \end{gathered}$ | $\begin{gathered} 2186 \\ 2391 \\ 4.6 / 11.5 \end{gathered}$ | $\begin{gathered} 2363 \\ 2496 \\ 4.8 / 12.0 \end{gathered}$ | $\begin{gathered} 3145 \\ 6.1 / 15.1 \end{gathered}$ | $\begin{gathered} 3843 \\ 7.4 / 18.5 \end{gathered}$ | $\begin{gathered} 4645 \\ 8.9 / 22.4 \end{gathered}$ | $\begin{gathered} 7966 \\ 15.3 / 38.3 \end{gathered}$ |
| 7 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) | $\begin{gathered} 197 \\ 292 \\ 672 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 431 \\ 643 \\ 1115 \\ 2.2 / 5.5 \end{gathered}$ | $\begin{gathered} 840 \\ 1256 \\ 1488 \\ 3.3 / 8.4 \end{gathered}$ | $\begin{gathered} 903 \\ 1349 \\ 1537 \\ 3.5 / 8.6 \end{gathered}$ | $\begin{gathered} 1488 \\ 1952 \\ 4.4 / 11.0 \\ \hline \end{gathered}$ | $\begin{gathered} 1614 \\ 2035 \\ 4.6 / 11.4 \\ \hline \end{gathered}$ | $\begin{gathered} 2423 \\ 2531 \\ 5.7 / 14.2 \end{gathered}$ | $\begin{gathered} 3052 \\ 6.9 / 17.1 \end{gathered}$ | $\begin{gathered} 3633 \\ 8.2 / 20.4 \end{gathered}$ | $\begin{gathered} 5866 \\ 13.2 / 32.9 \end{gathered}$ |
| 8 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) | $\begin{gathered} 134 \\ 198 \\ 514 \\ 1.5 / 3.5 \end{gathered}$ | $\begin{gathered} 296 \\ 440 \\ 867 \\ 1.9 / 4.8 \end{gathered}$ | $\begin{gathered} 585 \\ 872 \\ 1268 \\ 3.0 / 7.6 \end{gathered}$ | $\begin{gathered} 629 \\ 939 \\ 1308 \\ 3.217 .9 \end{gathered}$ | 1052 1572 1649 $4.2 / 10.6$ | $\begin{gathered} 1144 \\ 1711 \\ 1717 \\ 4.4 / 11.0 \end{gathered}$ | $\begin{gathered} 1746 \\ 2117 \\ 5.4 / 13.6 \end{gathered}$ | $\begin{gathered} 2423 \\ 2530 \\ 6.5 / 16.2 \end{gathered}$ | $\begin{gathered} 2983 \\ 7.7 / 19.1 \end{gathered}$ | $\begin{gathered} 4642 \\ 11.9 / 29.8 \end{gathered}$ |
| 9 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) | $\begin{gathered} 95 \\ 140 \\ 406 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 211 \\ 313 \\ 684 \\ 1.7 / 4.2 \\ \hline \end{gathered}$ | $\begin{gathered} 422 \\ 628 \\ 1086 \\ 2.7 / 6.7 \end{gathered}$ | $\begin{gathered} 454 \\ 677 \\ 1139 \\ 2.877 .1 \\ \hline \end{gathered}$ | $\begin{gathered} 768 \\ 1146 \\ 1428 \\ 4.1 / 10.1 \\ \hline \end{gathered}$ | $\begin{gathered} 837 \\ 1250 \\ 1484 \\ 4.3 / 10.7 \\ \hline \end{gathered}$ | $\begin{gathered} 1293 \\ 1820 \\ 5.3 / 13.1 \\ \hline \end{gathered}$ | $\begin{gathered} 1816 \\ 2161 \\ 6.2 / 15.6 \end{gathered}$ | $\begin{gathered} 2423 \\ 2529 \\ 7.3 / 18.3 \end{gathered}$ | $\begin{gathered} 3839 \\ 11.1 / 27.7 \end{gathered}$ |
| 10 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) | $\begin{gathered} \hline 70 \\ 102 \\ 328 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 156 \\ 230 \\ 554 \\ 1.5 / 3.8 \end{gathered}$ | $\begin{gathered} 313 \\ 465 \\ 878 \\ 2.4 / 6.0 \end{gathered}$ | $\begin{gathered} 338 \\ 502 \\ 924 \\ 2.5 / 6.3 \end{gathered}$ | $\begin{gathered} 576 \\ 858 \\ 1258 \\ 3.6 / 9.1 \\ \hline \end{gathered}$ | $\begin{gathered} 629 \\ 938 \\ 1307 \\ 3.9 / 9.7 \\ \hline \end{gathered}$ | $\begin{gathered} 981 \\ 1464 \\ 1595 \\ 5.1 / 12.8 \end{gathered}$ | $\begin{gathered} 1390 \\ 1885 \\ 6.1 / 15.1 \end{gathered}$ | $\begin{gathered} 1873 \\ 2195 \\ 7.0 / 17.6 \\ \hline \end{gathered}$ | $\begin{gathered} 3273 \\ 10.5 / 26.3 \end{gathered}$ |
| 11 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  | $\begin{gathered} 118 \\ 174 \\ 457 \\ 1.5 / 3.5 \end{gathered}$ | $\begin{gathered} 239 \\ 354 \\ 725 \\ 2.2 / 5.5 \end{gathered}$ | $\begin{gathered} 258 \\ 382 \\ 763 \\ 2.3 / 5.8 \end{gathered}$ | $\begin{gathered} 442 \\ 658 \\ 1095 \\ 3.3 / 8.3 \end{gathered}$ | $\begin{gathered} 484 \\ 719 \\ 1164 \\ 3.5 / 8.8 \end{gathered}$ | $\begin{gathered} 760 \\ 1132 \\ 1420 \\ 4.8 / 12.0 \end{gathered}$ | $\begin{gathered} 1085 \\ 1619 \\ 1672 \\ 5.9 / 14.8 \end{gathered}$ | $\begin{gathered} 1473 \\ 1939 \\ 6.8 / 17.1 \end{gathered}$ | $\begin{gathered} 2852 \\ 10.1 / 25.2 \end{gathered}$ |
| 12 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  | $\begin{gathered} 92 \\ 134 \\ 383 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 186 \\ 275 \\ 609 \\ 2.0 / 5.0 \\ \hline \end{gathered}$ | $\begin{gathered} 201 \\ 297 \\ 640 \\ 2.1 / 5.3 \\ \hline \end{gathered}$ | $\begin{gathered} 346 \\ 514 \\ 919 \\ 3.0 / 7.6 \\ \hline \end{gathered}$ | 379 563 977 $3.2 / 8.1$ | 599 892 1279 $4.4 / 11.0$ | $\begin{gathered} 861 \\ 1283 \\ 1501 \\ 5.7 / 14.2 \end{gathered}$ | $\begin{gathered} 1176 \\ 1736 \\ 6.7 / 16.7 \end{gathered}$ | $\begin{gathered} 2423 \\ 2526 \\ 9.7 / 24.3 \end{gathered}$ |
| 13 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  | $\begin{gathered} 73 \\ 105 \\ 326 \\ 1.5 / 3.5 \end{gathered}$ | $\begin{gathered} 148 \\ 217 \\ 518 \\ 1.9 / 4.6 \end{gathered}$ | $\begin{gathered} 160 \\ 235 \\ 545 \\ 1.9 / 4.9 \end{gathered}$ | $\begin{gathered} 276 \\ 408 \\ 783 \\ 2.8 / 7.0 \end{gathered}$ | $\begin{gathered} 302 \\ 448 \\ 832 \\ 3.0 / 7.4 \\ \hline \end{gathered}$ | 480 713 1136 $4.1 / 10.1$ | $\begin{gathered} 694 \\ 1032 \\ 1362 \\ 5.2 / 13.1 \\ \hline \end{gathered}$ | $\begin{gathered} 952 \\ 1419 \\ 1571 \\ 6.5 / 16.3 \end{gathered}$ | $\begin{gathered} 1994 \\ 2267 \\ 9.5 / 23.7 \end{gathered}$ |
| 14 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  | 58 84 281 $1.5 / 3.5$ | $\begin{gathered} 119 \\ 174 \\ 446 \\ 1.7 / 4.3 \end{gathered}$ | $\begin{gathered} 129 \\ 188 \\ 469 \\ 1.8 / 4.5 \end{gathered}$ | $\begin{gathered} \hline 223 \\ 329 \\ 674 \\ 2.6 / 6.5 \end{gathered}$ | 245 361 716 $2.8 / 6.9$ | 390 579 979 $3.8 / 9.4$ | 566 841 1247 $4.8 / 12.1$ | $\begin{gathered} 781 \\ 1162 \\ 1435 \\ 6.1 / 15.1 \end{gathered}$ | $\begin{gathered} 1657 \\ 2056 \\ 9.2 / 23.1 \end{gathered}$ |
| 15 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  | $\begin{gathered} 48 \\ 68 \\ 244 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 97 \\ 141 \\ 388 \\ 1.6 / 4.0 \\ \hline \end{gathered}$ | $\begin{gathered} 105 \\ 153 \\ 408 \\ 1.7 / 4.2 \\ \hline \end{gathered}$ | $\begin{gathered} 183 \\ 269 \\ 586 \\ 2.4 / 6.0 \end{gathered}$ | $\begin{gathered} 201 \\ 296 \\ 623 \\ 2.6 / 6.4 \\ \hline \end{gathered}$ | 321 475 852 $3.5 / 8.8$ | $\begin{gathered} 468 \\ 694 \\ 1097 \\ 4.5 / 11.3 \end{gathered}$ | $\begin{gathered} 647 \\ 962 \\ 1321 \\ 5.6 / 14.1 \\ \hline \end{gathered}$ | $\begin{gathered} 1390 \\ 1881 \\ 9.1 / 22.7 \end{gathered}$ |
| 16 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  | $\begin{gathered} 81 \\ 116 \\ 340 \\ 1.5 / 3.7 \end{gathered}$ | $\begin{gathered} 87 \\ 126 \\ 358 \\ 1.6 / 3.9 \end{gathered}$ | $\begin{gathered} 152 \\ 222 \\ 515 \\ 2.3 / 5.7 \end{gathered}$ | $\begin{gathered} 167 \\ 244 \\ 547 \\ 2.4 / 6.0 \\ \hline \end{gathered}$ | 268 394 748 $3.3 / 8.2$ | 390 578 963 $4.2 / 10.6$ | $\begin{gathered} 542 \\ 804 \\ 1204 \\ 5.3 / 13.2 \end{gathered}$ | $\begin{gathered} 1176 \\ 1733 \\ 8.9 / 22.3 \\ \hline \end{gathered}$ |
| 17 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  | $\begin{gathered} 67 \\ 97 \\ 301 \\ 1.5 / 3.5 \end{gathered}$ | $\begin{gathered} 73 \\ 105 \\ 317 \\ 1.5 / 3.7 \end{gathered}$ | $\begin{gathered} 128 \\ 186 \\ 455 \\ 2.1 / 5.3 \end{gathered}$ | $\begin{gathered} 140 \\ 204 \\ 484 \\ 2.3 / 5.7 \end{gathered}$ | 225 331 661 $3.1 / 7.7$ | $\begin{gathered} 329 \\ 486 \\ 852 \\ 4.0 / 9.9 \end{gathered}$ | $\begin{gathered} 458 \\ 678 \\ 1066 \\ 5.0 / 12.4 \end{gathered}$ | $\begin{gathered} 1003 \\ 1492 \\ 1607 \\ 8.6 / 21.5 \end{gathered}$ |
| 18 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  | $\begin{gathered} 57 \\ 81 \\ 268 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 62 \\ 88 \\ 282 \\ 1.5 / 3.5 \\ \hline \end{gathered}$ | $\begin{gathered} 108 \\ 156 \\ 405 \\ 2.0 / 5.0 \end{gathered}$ | $\begin{gathered} 119 \\ 172 \\ 431 \\ 2.1 / 5.3 \\ \hline \end{gathered}$ | $\begin{gathered} 191 \\ 279 \\ 589 \\ 2.9 / 7.3 \\ \hline \end{gathered}$ | $\begin{gathered} 280 \\ 412 \\ 759 \\ 3.8 / 9.4 \\ \hline \end{gathered}$ | $\begin{gathered} 390 \\ 577 \\ 949 \\ 4.7 / 11.7 \end{gathered}$ | $\begin{gathered} 861 \\ 1279 \\ 1497 \\ 8.1 / 20.3 \\ \hline \end{gathered}$ |
| 19 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  | $\begin{gathered} 53 \\ 74 \\ 253 \\ 1.5 / 3.5 \end{gathered}$ | $\begin{gathered} 92 \\ 133 \\ 363 \\ 1.9 / 4.7 \end{gathered}$ | $\begin{gathered} 101 \\ 146 \\ 386 \\ 2.0 / 5.0 \\ \hline \end{gathered}$ | $\begin{gathered} 163 \\ 238 \\ 528 \\ 2.8 / 6.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 240 \\ 352 \\ 681 \\ 3.6 / 8.9 \\ \hline \end{gathered}$ | 335 494 851 $4.4 / 11.1$ | $\begin{gathered} 744 \\ 1104 \\ 1402 \\ 7.7 / 19.2 \\ \hline \end{gathered}$ |
| 20 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  | $\begin{gathered} 79 \\ 113 \\ 327 \\ 1.8 / 4.5 \end{gathered}$ | 87 125 348 $1.9 / 4.8$ | 141 204 476 $2.6 / 6.5$ | $\begin{gathered} 207 \\ 303 \\ 613 \\ 3.4 / 8.4 \end{gathered}$ | $\begin{gathered} 290 \\ 426 \\ 767 \\ 4.2 / 10.5 \end{gathered}$ | $\begin{gathered} 647 \\ 959 \\ 1318 \\ 7.3 / 18.2 \end{gathered}$ |
| 21 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  | $\begin{gathered} 69 \\ 97 \\ 296 \\ 1.7 / 4.3 \\ \hline \end{gathered}$ | 76 107 315 $1.8 / 4.5$ | $\begin{gathered} 122 \\ 176 \\ 431 \\ 2.5 / 6.2 \\ \hline \end{gathered}$ | $\begin{gathered} 180 \\ 262 \\ 556 \\ 3.2 / 8.0 \\ \hline \end{gathered}$ | $\begin{gathered} 252 \\ 370 \\ 695 \\ 4.0 / 10.0 \end{gathered}$ | $\begin{gathered} 566 \\ 837 \\ 1200 \\ 6.9 / 17.3 \\ \hline \end{gathered}$ |
| 22 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  | 60 84 270 $1.6 / 4.1$ | $\begin{gathered} 66 \\ 93 \\ 287 \\ 1.7 / 4.3 \\ \hline \end{gathered}$ | $\begin{gathered} 107 \\ 153 \\ 392 \\ 2.4 / 5.9 \\ \hline \end{gathered}$ | $\begin{gathered} 157 \\ 228 \\ 506 \\ 3.1 / 7.6 \\ \hline \end{gathered}$ | $\begin{gathered} 221 \\ 322 \\ 633 \\ 3.8 / 9.6 \\ \hline \end{gathered}$ | $\begin{gathered} 498 \\ 735 \\ 1093 \\ 6.6 / 16.5 \end{gathered}$ |
| 23 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  |  | $\begin{gathered} 58 \\ 81 \\ 262 \\ 1.7 / 4.1 \end{gathered}$ | 94 134 358 $2.3 / 5.7$ | $\begin{gathered} 138 \\ 200 \\ 462 \\ 2.9 / 7.3 \end{gathered}$ | $\begin{gathered} 194 \\ 283 \\ 578 \\ 3.7 / 9.1 \end{gathered}$ | 440 648 999 $6.3 / 15.8$ |
| 24 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  |  |  | $\begin{gathered} 83 \\ 117 \\ 328 \\ 2.2 / 5.4 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 122 \\ 175 \\ 424 \\ 2.877 .0 \\ \hline \end{gathered}$ | $\begin{gathered} 172 \\ 249 \\ 530 \\ 3.5 / 8.7 \\ \hline \end{gathered}$ | 390 574 916 $6.0 / 15.1$ |
| 26 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  |  |  | $\begin{gathered} 65 \\ 91 \\ 279 \\ 2.0 / 5.0 \\ \hline \end{gathered}$ | $\begin{gathered} 97 \\ 137 \\ 360 \\ 2.6 / 6.4 \\ \hline \end{gathered}$ | $\begin{gathered} 136 \\ 196 \\ 450 \\ 3.2 / 8.0 \\ \hline \end{gathered}$ | $\begin{gathered} 312 \\ 455 \\ 779 \\ 5.6 / 13.9 \\ \hline \end{gathered}$ |
| 28 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  |  |  | 53 72 239 $1.8 / 4.6$ | $\begin{gathered} 78 \\ 109 \\ 309 \\ 2.4 / 5.9 \end{gathered}$ | $\begin{gathered} 110 \\ 156 \\ 387 \\ 3.0 / 7.4 \end{gathered}$ | $\begin{gathered} 252 \\ 367 \\ 670 \\ 5.2 / 12.9 \end{gathered}$ |
| 30 | Unfactored Load (LL) L/360 <br> Unfactored Load (TL) L/240 <br> Factored Total Load <br> Min. End / Int. Bearing (in) |  |  |  |  |  |  |  | $\begin{gathered} 64 \\ 87 \\ 268 \\ 2.2 / 5.5 \end{gathered}$ | $\begin{gathered} 90 \\ 126 \\ 336 \\ 2.8 / 6.9 \end{gathered}$ | 207 299 582 $4.8 / 12.0$ |

[^1]Verify adequacy of beam in uniform load tables prior to using values listed below.
$3100 \mathrm{~F}_{\mathrm{b}}-2.0 \mathrm{E} 13 / 4^{\prime \prime}$ WEST FRASER $^{\text {TM }}$ LVL


* 4-ply beams should only be side-loaded when loads are applied to both sides of the member.

1. Nails to be located a minimum of 2 " from the top and bottom of the member. Start all nails a minimum of $21 / 2^{\prime \prime}$ in from ends.
2. Bolts are to be material conforming to ASTM Standard A307. Bolt holes are to be the same diameter as the bolt, and located $2^{\prime \prime}$ from the top and bottom of the member. Washers should be used under head and nut. Start all bolts a minimum of $21 / 2^{\prime \prime}$ in from ends.
3. Values listed are for standard term loading.

EXAMPLE (All loads shown are total factored)
First, convert joist reactions to plf load on each side of the beam by taking the joist reaction (lbs.) divided by the joist spacing (ft.). $400 \mathrm{lbs} /(16 / 12)=300 \mathrm{plf}$ and $533 \mathrm{lbs} /(16 / 12)=400$ plf. Check factored resistance tables to verify that 3 plys can carry the total factored load of 700 plf. The maximum load applied to either outside member is 400 plf. Use 2 rows of $16 \mathrm{~d}\left(3^{1 / 2 "}\right)$ common wire nails at $12^{\prime \prime}$ o.c. (good for 663 plf ).


CONNECTION OF MULTIPLE PIECES FOR TOP-LOADED BEAMS
2.0E ( $13 / 4^{\prime \prime}$ wide pieces)

- Minimum of 2 rows of $16 \mathrm{~d}\left(3^{1 / 2} 2^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $51 / 2^{\prime \prime}$ through $117 / 8^{\prime \prime}$ beams
- Minimum of 3 rows of $16 \mathrm{~d}\left(31 / 2^{\prime \prime}\right)$ nails at $12^{\prime \prime} 0 . c$. for $14^{\prime \prime}$ through $24^{\prime \prime}$ beams



## NOTES



## DESIGN PROPERTIES

$3000 \mathrm{~F}_{\mathrm{b}}-1.9 \mathrm{E} 13 / 4^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91/2" | 111/2" | 117/8" | 14" | 16" | 18" | 24" |
| Moment (ft.lbs.) | 4079 | 6827 | 10751 | 11299 | 16132 | 17126 | 23277 | 29855 | 37184 | 63568 |
| Shear (lbs.) | 3199 | 4217 | 5381 | 5526 | 6690 | 6908 | 8144 | 9307 | 10471 | 13961 |
| Moment of Inertia (in^4) | 24 | 56 | 115 | 125 | 222 | 244 | 400 | 597 | 851 | 2016 |
| Weight (lbs./lin.ft.) | 2.7 | 3.6 | 4.6 | 4.7 | 5.7 | 5.9 | 7.0 | 8.0 | 9.0 | 12.0 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. Lateral support of beam is required at bearing locations.
3. All $16^{\prime \prime}$ and greater beam depths are to be used in multiple member units only.
$3000 \mathrm{~F}_{\mathrm{b}}-1.9 \mathrm{E} 13 / 4^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL AVAILABLE SIZES*

$3000 \mathrm{~F}_{\mathrm{b}}-1.9 \mathrm{E}$ WEST FRASER ${ }^{T M}$ LVL SPECIFIED STRENGTHS (STANDARD TERM)
[^2]| E | $=1.9 \times 10 \wedge 6 \mathrm{psi}$ |
| ---: | :--- |
| Fb | $=5544 \mathrm{psi}$ |
| FV | $=554 \mathrm{psi}$ |
| $\mathrm{Fc}($ perp $)$ | $=1300 \mathrm{psi}$ |
| $\mathrm{Fc}($ para $)$ | $=4000 \mathrm{psi}$ |

## GENERAL NOTES

- Tables are for one-ply $13 / 4^{\prime \prime}$ beams. When properly connected, double the values for two-ply beams, triple for three. Minimum bearing lengths shown for one-ply will be the same for two-ply and three-ply. See page 15 for multiple-ply connection details.
- Resistances shown are the maximum factored and/or unfactored resistances, in pounds per lineal foot, that can be applied to the beam in addition to its own weight.
- Tables are based on uniform loads and the most restrictive of simple or continuous spans and dry-use conditions. Refer to West Fraser's sizing software for other loads or span configurations.
- Lateral support of beam compression edges is required at intervals of $24^{\prime \prime}$ o/c or closer.
- Lateral support of beams is required at bearing locations.
- West Fraser ${ }^{\text {rM }}$ LVL beams are made without camber; therefore, in addition to complying with the deflection limits of the applicable building code, other deflection considerations, such as long term deflection under sustained loads (including creep), must be evaluated.
- All $16^{\prime \prime}$ and deeper beams are to be used in multiple member units only.
- Unfactored total load resistance is limited to a deflection of L/240. Unfactored live load resistance is based on a deflection of L/360. Check local code requirements for other deflection criteria.
- For an unfactored live load deflection limit of L/480, multiply UNFACTORED LOAD L/360 resistance by 0.75 .
- Roof must have positive slope in order to prevent ponding.
- Spans of multiple spans must be at least $40 \%$ of adjacent span.
- Bearing lengths are based on 1300 psi specified strength for 1.9E Grade materials which cannot be increased for duration of load. Bearing length may need to be increased if support member's allowable bearing stress is less.
- Tables will accommodate beam slopes to a maximum of 2:12.


## INSTRUCTIONS FOR USE

1. Determine the factored total load and unfactored total and live load on the beam in pounds per lineal foot (plf).
2. Locate a span that meets or exceeds the required beam span, centre-to-centre of bearing.
3. Scan from left to right within the SPAN row until you find a cell where; (1) the UNFACTORED LOAD L/360 resistance meets or exceeds the unfactored live load, (2) the UNFACTORED LOAD L/240 resistance meets or exceeds the unfactored total load and (3) the FACTORED TOTAL LOAD resistance meets or exceeds the factored total load. All three rows must be checked and satisfied. Where no unfactored resistances are shown, factored total load will control.
4. To size a member for a span not shown, use capacities for the next larger span shown.

FACTORED RESISTANCE TABLE (pounos perlineal foot)
$3000 \mathrm{Fb}_{\mathrm{b}}$-1.9E West Fraser ${ }^{\text {tw }}$ LVL - FLOOR or ROOF (Standard Term)

| Span (ft) |  | 13/4" WIDTH |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Depth | 5-1/2" | 7-1/4" | 9-1/4" | 9-1/2" | 11-1/2" | 11-7/8" | $14{ }^{\prime \prime}$ | $16^{\prime \prime}$ | 18" | 24" |
| 6 | Unfactored Load (LL) L/360 | 290 | 627 | 1200 | 1286 | 2077 | 2245 |  |  |  |  |
|  | Unfactored Load (TL) L/240 | 433 | 936 | 1795 |  |  |  |  |  |  |  |
|  | Factored Total Load | 904 | 1337 | 1802 | 1863 | 2391 | 2496 | 3145 | 3843 | 4645 | 7966 |
|  | Min. End / Int. Bearing (in) | 1.5/3.7 | 2.5/6.2 | 3.5/8.7 | 3.6/9.0 | 4.6/11.5 | 4.8/12.0 | 6.1/15.1 | 7.4/18.5 | 8.9/22.4 | 15.3/38.3 |
| 7 | Unfactored Load (LL) L/360 | 187 | 409 | 798 | 858 | 1413 | 1533 | 2302 |  |  |  |
|  | Unfactored Load (TL) L/240 | 277 | 610 | 1193 | 1282 |  |  |  |  |  |  |
|  | Factored Total Load | 663 | 1111 | 1488 | 1537 | 1952 | 2035 | 2531 | 3052 | 3633 | 5866 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 2.1/5.3 | 3.3/8.4 | 3.5/8.6 | 4.4/11.0 | 4.6/11.4 | 5.7/14.2 | 6.9/17.1 | 8.2/20.4 | 13.2/32.9 |
| 8 | Unfactored Load (LL) L/360 | 127 | 281 | 555 | 598 | 999 | 1087 | 1658 | 2302 |  |  |
|  | Unfactored Load (TL) L/240 | 188 | 418 | 828 | 892 | 1493 | 1625 |  |  |  |  |
|  | Factored Total Load | 507 | 850 | 1268 | 1308 | 1649 | 1717 | 2117 | 2530 | 2983 | 4642 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.9/4.7 | 2.9/7.4 | 3.1/7.7 | 4.2/10.6 | 4.4/11.0 | 5.4/13.6 | 6.5/16.2 | 7.7/19.1 | 11.9/29.8 |
| 9 | Unfactored Load (LL) L/360 | 90 | 201 | 401 | 431 | 729 | 795 | 1228 | 1725 | 2302 |  |
|  | Unfactored Load (TL) L/240 | 132 | 297 | 596 | 643 | 1088 | 1187 |  |  |  |  |
|  | Factored Total Load | 400 | 671 | 1057 | 1111 | 1428 | 1484 | 1820 | 2161 | 2529 | 3839 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.714.1 | 2.6/6.5 | 2.7/6.9 | 3.9/9.8 | 4.2/10.4 | 5.3/13.1 | 6.2/15.6 | 7.3/18.3 | 11.1/27.7 |
| 10 | Unfactored Load (LL) L/360 | 66 | 148 | 298 | 321 | 547 | 598 | 932 | 1321 | 1779 |  |
|  | Unfactored Load (TL) L/240 | 97 | 219 | 442 | 477 | 815 | 890 | 1390 |  |  |  |
|  | Factored Total Load | 324 | 543 | 855 | 899 | 1258 | 1307 | 1595 | 1885 | 2195 | 3273 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.5/3.7 | 2.3/5.9 | 2.5/6.2 | 3.5/8.8 | 3.7/9.4 | 5.1/12.7 | 6.1/15.1 | 7.0/17.6 | 10.5/26.3 |
| 11 | Unfactored Load (LL) L/360 |  | 112 | 227 | 245 | 420 | 459 | 722 | 1031 | 1399 | 2828 |
|  | Unfactored Load (TL) L/240 |  | 165 | 336 | 363 | 624 | 683 | 1075 | 1538 |  |  |
|  | Factored Total Load |  | 448 | 706 | 742 | 1061 | 1126 | 1420 | 1672 | 1939 | 2852 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 2.1/5.3 | 2.2/5.6 | 3.2/8.0 | 3.4/8.5 | 4.6/11.6 | 5.9/14.8 | 6.8/17.1 | 10.1/25.2 |
| 12 | Unfactored Load (LL) L/360 |  | 87 | 177 | 191 | 329 | 360 | 569 | 818 | 1117 | 2302 |
|  | Unfactored Load (TL) L/240 |  | 127 | 261 | 282 | 488 | 534 | 847 | 1219 | 1667 |  |
|  | Factored Total Load |  | 376 | 593 | 623 | 890 | 946 | 1279 | 1501 | 1736 | 2526 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 2.014.9 | 2.1/5.1 | 2.9/7.3 | 3.1/7.8 | 4.2/10.6 | 5.4/13.6 | 6.7/16.7 | 9.7/24.3 |
| 13 | Unfactored Load (LL) L/360 |  | 69 | 140 | 152 | 262 | 287 | 456 | 659 | 905 | 1894 |
|  | Unfactored Load (TL) L/240 |  | 100 | 206 | 223 | 388 | 425 | 677 | 980 | 1348 |  |
|  | Factored Total Load |  | 320 | 504 | 530 | 758 | 805 | 1095 | 1362 | 1571 | 2267 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.8/4.5 | 1.9/4.7 | 2.7/6.8 | 2.9/7.2 | 3.9/9.8 | 5.0/12.5 | 6.3/15.6 | 9.5/23.7 |
| 14 | Unfactored Load (LL) L/360 |  | 55 | 113 | 122 | 212 | 233 | 371 | 538 | 742 | 1574 |
|  | Unfactored Load (TL) L/240 |  | 80 | 165 | 179 | 313 | 343 | 549 | 799 | 1104 |  |
|  | Factored Total Load |  | 275 | 434 | 456 | 653 | 693 | 943 | 1211 | 1435 | 2056 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.7/4.2 | 1.8/4.4 | 2.5/6.3 | 2.7/6.7 | 3.6/9.1 | 4.7/11.6 | 5.8/14.5 | 9.2/23.1 |
| 15 | Unfactored Load (LL) L/360 |  | 45 | 93 | 100 | 174 | 191 | 305 | 444 | 615 | 1321 |
|  | Unfactored Load (TL) L/240 |  | 64 | 134 | 145 | 255 | 280 | 451 | 658 | 913 |  |
|  | Factored Total Load |  | 239 | 378 | 397 | 568 | 603 | 821 | 1054 | 1313 | 1881 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.6/3.9 | 1.6/4.1 | 2.3/5.9 | 2.5/6.2 | 3.4/8.5 | 4.3/10.9 | 5.4/13.5 | 9.1/22.7 |
| 16 | Unfactored Load (LL) L/360 |  |  | 77 | 83 | 144 | 159 | 254 | 371 | 515 | 1117 |
|  | Unfactored Load (TL) L/240 |  |  | 110 | 119 | 211 | 232 | 374 | 548 | 763 | 1664 |
|  | Factored Total Load |  |  | 331 | 348 | 498 | 529 | 720 | 925 | 1153 | 1733 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.6 | 1.5/3.8 | 3.2/5.5 | 2.3/5.8 | 3.2/7.9 | 4.1/10.2 | 5.1/12.7 | 8.7/21.7 |
| 17 | Unfactored Load (LL) L/360 |  |  | 64 | 69 | 121 | 133 | 214 | 313 | 435 | 953 |
|  | Unfactored Load (TL) L/240 |  |  | 92 | 99 | 176 | 194 | 314 | 461 | 644 | 1417 |
|  | Factored Total Load |  |  | 293 | 308 | 441 | 468 | 637 | 818 | 1020 | 1607 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.6 | 2.1/5.1 | 2.2/5.5 | 3.0/7.4 | 3.8/9.6 | 4.8/11.9 | 8.2/20.4 |
| 18 | Unfactored Load (LL) L/360 |  |  | 54 | 59 | 103 | 113 | 181 | 266 | 371 | 818 |
|  | Unfactored Load (TL) L/240 |  |  | 77 | 83 | 148 | 163 | 265 | 391 | 547 | 1215 |
|  | Factored Total Load |  |  | 261 | 274 | 393 | 417 | 568 | 729 | 909 | 1497 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.5 | 1.9/4.9 | 2.1/5.2 | 2.8/7.0 | 3.6/9.0 | 4.5/11.2 | 7.7/19.3 |
| 19 | Unfactored Load (LL) L/360 |  |  |  | 50 | 88 | 96 | 155 | 228 | 319 | 707 |
|  | Unfactored Load (TL) L/240 |  |  |  | 70 | 126 | 138 | 226 | 334 | 469 | 1049 |
|  | Factored Total Load |  |  |  | 246 | 352 | 374 | 509 | 654 | 815 | 1397 |
|  | Min. End / Int. Bearing (in) |  |  |  | 1.5/3.5 | 1.8/4.6 | 2.0/4.9 | 2.7/6.6 | 3.4/8.5 | 4.3/10.6 | 7.3/18.2 |
| 20 | Unfactored Load (LL) L/360 |  |  |  |  | 75 | 83 | 134 | 197 | 275 | 615 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 107 | 118 | 194 | 287 | 404 | 910 |
|  | Factored Total Load |  |  |  |  | 317 | 337 | 459 | 589 | 735 | 259 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.7/4.4 | 1.9/4.6 | 2.5/6.3 | 3.2/8.1 | 4.0/10.1 | 6.9/17.3 |
| 21 | Unfactored Load (LL) L/360 |  |  |  |  | 65 | 72 | 116 | 171 | 240 | 538 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 92 | 102 | 167 | 248 | 351 | 795 |
|  | Factored Total Load |  |  |  |  | 287 | 305 | 415 | 534 | 666 | 1141 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.714.1 | 1.8/4.4 | 2.4/6.0 | 3.1/7.7 | 3.8/9.6 | 6.6/16.5 |
| 22 | Unfactored Load (LL) L/360 |  |  |  |  | 57 | 63 | 101 | 149 | 210 | 473 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 80 | 88 | 145 | 216 | 306 | 697 |
|  | Factored Total Load |  |  |  |  | 261 | 277 | 378 | 485 | 606 | 1039 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.6/3.9 | 1.7/4.2 | 2.3/5.7 | 2.9/7.3 | 3.7/9.2 | 6.3/15.7 |
| 23 | Unfactored Load (LL) L/360 |  |  |  |  |  | 55 | 89 | 131 | 185 | 418 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  | 76 | 127 | 189 | 268 | 615 |
|  | Factored Total Load |  |  |  |  |  | 253 | 345 | 444 | 553 | 949 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  | 1.6/4.0 | 2.2/5.4 | 2.817.0 | 3.5/8.7 | 6.0/15.0 |
| 24 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 79 | 116 | 163 | 371 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 111 | 166 | 236 | 544 |
|  | Factored Total Load |  |  |  |  |  |  | 316 | 407 | 507 | 871 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 2.1/5.2 | 2.716.7 | 3.3/8.4 | 5.7/14.4 |
| 26 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 62 | 92 | 130 | 296 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 86 | 130 | 185 | 432 |
|  | Factored Total Load |  |  |  |  |  |  | 268 | 345 | 431 | 740 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.9/4.8 | 2.5/6.2 | 3.1/7.7 | 5.3/13.2 |
| 28 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 50 | 74 | 104 | 240 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 68 | 103 | 148 | 348 |
|  | Factored Total Load |  |  |  |  |  |  | 231 | 297 | 370 | 637 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.8/4.4 | 2.3/5.7 | 2.8/7.1 | 4.9/12.3 |
| 30 | Unfactored Load (LL) L/360 |  |  |  |  |  |  |  | 60 | 85 | 197 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  |  | 83 | 119 | 283 |
|  | Factored Total Load |  |  |  |  |  |  |  | 257 | 322 | 553 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  |  | 2.1/5.3 | 2.716.6 | 4.6/11.4 |

Verify adequacy of beam in uniform load tables prior to using values listed below.
$3000 \mathrm{~F}_{\mathrm{b}}-1.9 \mathrm{E} 13 / 4^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL

| Maximum Factored Uniform Load (PLF) Applied to Either Outside Member |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Connector | Spacing | Rows | Nails On One Side or Through Bolts | Nails Both Sides or Through Bolts | Through Bolts Only |  |
| 16d ( $3^{1 ⁄ 2 "}$ ") <br> Common Wire Nails | 12" o.c. | 2 Rows <br> 3 Rows | $\begin{gathered} 827 \\ 1241 \end{gathered}$ | $\begin{aligned} & 620 \\ & 930 \end{aligned}$ | Not Applicable |  |
|  | 6" o.c. | 2 Rows <br> 3 Rows | $\begin{aligned} & 1654 \\ & 2482 \end{aligned}$ | $\begin{aligned} & 1240 \\ & 1860 \end{aligned}$ | Not Applicable |  |
|  | 4" o.c. | 2 Rows <br> 3 Rows | $\begin{aligned} & 2481 \\ & 3723 \end{aligned}$ | $\begin{aligned} & 1860 \\ & 2790 \end{aligned}$ | Not Applicable |  |
| 1⁄2" A307 | 24" о.c. | 2 Rows | 671 | 503 | 448 |  |
| Through | 12" о.c. | 2 Rows | 1342 | 1006 | 895 |  |
| B | 6" o.c. | 2 Rows | 2684 | 2012 | 1790 |  |

* 4-ply beams should only be side-loaded when loads are applied to both sides of the member.

1. Nails to be located a minimum of $2^{\prime \prime}$ from the top and bottom of the member. Start all nails a minimum of $21 / 2^{\prime \prime}$ in from ends.
2. Bolts are to be material conforming to ASTM Standard A307. Bolt holes are to be the same diameter as the bolt, and located 2" from the top and bottom of the member. Washers should be used under head and nut. Start all bolts a minimum of $21 / 2^{\prime \prime}$ in from ends.
3. Values listed are for standard term loading.

EXAMPLE (All loads shown are total factored)
First, convert joist reactions to plf load on each side of the beam by taking the joist reaction (lbs.) divided by the joist spacing (ft.). $400 \mathrm{lbs} /(16 / 12)=300 \mathrm{plf}$ and $533 \mathrm{lbs} /(16 / 12)=400$ plf. Check factored resistance tables to verify that 3 plys can carry the total factored load of 700 plf. The maximum load applied to either outside member is 400 plf. Use 2 rows of $16 \mathrm{~d}\left(31^{1 / 2 \prime}\right)$ common wire nails at $12^{\prime \prime}$ o.c. (good for 620 plf ).


CONNECTION OF MULTIPLE PIECES FOR TOP-LOADED BEAMS
1.9 E ( $13 / 4^{\prime \prime}$ wide pieces)

- Minimum of 2 rows of $16 \mathrm{~d}\left(3^{1} / 2^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $51 / 2^{\prime \prime}$ through $117 / 8^{\prime \prime}$ beams
- Minimum of 3 rows of $16 d\left(31 / 2^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $14^{\prime \prime}$ through $24^{\prime \prime}$ beams



## NOTES



## EJ <br> Uest froser LVL

## LVL 3000 Fb - $1.8 \mathrm{E} \quad 1 \frac{1}{2} 2^{\prime \prime}$ THICK

HEADERS AND BEAMS

## DESIGN PROPERTIES

$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E} 11 / 2^{\prime \prime}$ WEST FRASER"' LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91/2" | 111/2" | 117\% ${ }^{\prime \prime}$ | 14" | 16" | 18" |
| Moment (ft.lbs.) | 3497 | 5852 | 9215 | 9684 | 13827 | 14679 | 19951 | 25590 | 31872 |
| Shear (lbs.) | 2653 | 3497 | 4462 | 4583 | 5548 | 5729 | 6754 | 7718 | 8683 |
| Moment of Inertia (in^4) | 21 | 48 | 99 | 107 | 190 | 209 | 343 | 512 | 729 |
| Weight (lbs./lin.ft.) | 2.1 | 2.8 | 3.6 | 3.7 | 4.4 | 4.6 | 5.4 | 6.2 | 6.9 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. All $14^{\prime \prime}$ and greater beam depths are to be used in multiple member units only ( $11 / 2^{\prime \prime}$ thick).
3. Lateral support of beam is required at bearing locations.
$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E} 11 / 2^{\prime \prime}$ WEST FRASER ${ }^{\text {Tm }}$ LVL AVAILABLE SIZES

$3000 \mathrm{~F}_{\mathrm{b}}-\mathbf{1} .8 \mathrm{E}$ WEST FRASER ${ }^{\text {TM }}$ LVL SPECIFIED STRENGTHS (STANDARD TERM)

| Modulus of Elasticity | E $=1.8 \times 10 \wedge 6 \mathrm{psi}$ <br> Bending Stress $\mathrm{F}_{\mathrm{b}}$$=5544 \mathrm{psi}$ |  |
| :--- | ---: | :--- |
| Shear (joist) | $\mathrm{F}_{\mathrm{V}}$ | $=536 \mathrm{psi}$ |
| Compression Perpendicular to Grain (joist) | $\mathrm{F}_{\mathrm{c}(\text { perp }}$ | $=1365 \mathrm{psi}$ |
| Compression Parallel to Grain | $\mathrm{F}_{\mathrm{c}}$ (para) | $=3750 \mathrm{psi}$ |

1. $F_{b}$ based on $12^{\prime \prime}$ depths. For other depths, multiply by (12/d)^(1/7.35) .
2. $\mathrm{F}_{\mathrm{C}(\text { perp })}$ and E shall not be increased for duration of load.

## GENERAL NOTES

- Tables are for one-ply $1 \frac{1}{2 \prime \prime}$ beams. When properly connected, double the values for two-ply beams, triple for three. Minimum bearing lengths shown for one-ply will be the same for two-ply and three-ply. See page 21 for multiple-ply connection details.
- Resistances shown are the maximum factored and/or unfactored resistances, in pounds per lineal foot, that can be applied to the beam in addition to its own weight.
- Tables are based on uniform loads and the most restrictive of simple or continuous spans and dry-use conditions. Refer to West Fraser's sizing software for other loads or span configurations.
- Lateral support of beam compression edges is required at intervals of $24^{\prime \prime}$ o/c or closer.
- Lateral support of beams is required at bearing locations.
- West Fraser ${ }^{\text {rM }}$ LVL beams are made without camber; therefore, in addition to complying with the deflection limits of the applicable building code, other deflection considerations, such as long term deflection under sustained loads (including creep), must be evaluated.
- All 14 " and deeper beams are to be used in multiple member units only.
- Unfactored total load resistance is limited to a deflection of $\mathrm{L} / 240$. Unfactored live load resistance is based on a deflection of L/360. Check local code requirements for other deflection criteria.
- For an unfactored live load deflection limit of L/480, multiply UNFACTORED LOAD L/360 resistance by 0.75 .
- Roof must have positive slope in order to prevent ponding.
- Spans of multiple spans must be at least $40 \%$ of adjacent span.
- Bearing lengths are based on 1365 psi specified strength for 1.8E Grade materials which cannot be increased for duration of load. Bearing length may need to be increased if support member's allowable bearing stress is less.
- Tables will accommodate beam slopes to a maximum of 2:12.


## INSTRUCTIONS FOR USE

1. Determine the factored total load and unfactored total and live load on the beam in pounds per lineal foot (plf).
2. Locate a span that meets or exceeds the required beam span, centre-to-centre of bearing.
3. Scan from left to right within the SPAN row until you find a cell where; (1) the UNFACTORED LOAD L/360 resistance meets or exceeds the unfactored live load, (2) the UNFACTORED LOAD L/240 resistance
meets or exceeds the unfactored total load and (3) the FACTORED TOTAL LOAD resistance meets or exceeds the factored total load. All three rows must be checked and satisfied. Where no unfactored resistances are shown, factored total load will control.
4. To size a member for a span not shown, use capacities for the next larger span shown.

FACTORED RESISTANCE TABLE (pounosper lineal foot)
$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E}$ West Fraser ${ }^{\text {tw }}$ LVL - FLOOR or ROOF (Standard Term)

| Span (ft) |  | 1112" WIDTH |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Depth | 5-1/2" | 7-1/4" | 9-1/4" | 9-1/2" | 11-1/2" | 11-7/8" | 14" | $16^{\prime \prime}$ | 18" |
| 6 | Unfactored Load (LL) L/360 | 236 | 509 | 974 | 1044 | 1686 | 1823 |  |  |  |
|  | Unfactored Load (TL) L/240 | 351 | 760 | 1458 |  |  |  |  |  |  |
|  | Factored Total Load | 775 | 1109 | 1494 | 1545 | 1983 | 2071 | 2609 | 3188 | 3852 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 2.0/5.1 | 2.7/6.8 | 2.8/7.1 | 3.6/9.1 | 3.8/9.5 | 4.8/11.9 | 5.8/14.6 | 7.1/17.6 |
| 7 | Unfactored Load (LL) L/360 | 152 | 332 | 648 | 696 | 1148 | 1245 | 1869 |  |  |
|  | Unfactored Load (TL) L/240 | 225 | 496 | 969 | 1041 |  |  |  |  |  |
|  | Factored Total Load | 569 | 925 | 1235 | 1275 | 1619 | 1688 | 2100 | 2531 | 3013 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 2.0/4.9 | 2.6/6.6 | 2.7/6.8 | 3.5/8.6 | 3.6/9.0 | 4.5/11.2 | 5.4/13.5 | 6.4/16.1 |
| 8 | Unfactored Load (LL) L/360 | 103 | 228 | 451 | 485 | 811 | 883 | 1347 | 1869 | 2466 |
|  | Unfactored Load (TL) L/240 | 153 | 339 | 673 | 724 | 1213 | 1320 |  |  |  |
|  | Factored Total Load | 435 | 729 | 1052 | 1085 | 1368 | 1424 | 1756 | 2099 | 2474 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.8/4.5 | 2.6/6.4 | 2.6/6.6 | 3.3/8.4 | 3.5/8.7 | 4.3/10.7 | 5.1/12.8 | 6.0/15.1 |
| 9 | Unfactored Load (LL) L/360 | 73 | 163 | 325 | 350 | 592 | 646 | 997 | 1401 | 1869 |
|  | Unfactored Load (TL) L/240 | 108 | 242 | 484 | 522 | 884 | 964 | 1491 |  |  |
|  | Factored Total Load | 343 | 575 | 907 | 945 | 1184 | 1231 | 1509 | 1792 | 2098 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.6/3.9 | 2.5/6.2 | 2.6/6.5 | 3.3/8.1 | 3.4/8.5 | 4.1/10.4 | 4.9/12.3 | 5.8/14.4 |
| 10 | Unfactored Load (LL) L/360 | 54 | 120 | 242 | 261 | 444 | 485 | 757 | 1072 | 1445 |
|  | Unfactored Load (TL) L/240 | 78 | 178 | 359 | 387 | 662 | 723 | 1129 |  |  |
|  | Factored Total Load | 278 | 465 | 734 | 771 | 1044 | 1084 | 1323 | 1564 | 1821 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.5/3.5 | 2.2/5.6 | 2.4/5.9 | 3.2/8.0 | 3.3/8.3 | 4.0/10.1 | 4.8/11.9 | 5.6/13.9 |
| 11 | Unfactored Load (LL) L/360 |  | 91 | 184 | 199 | 341 | 373 | 586 | 837 | 1136 |
|  | Unfactored Load (TL) L/240 |  | 134 | 273 | 295 | 507 | 555 | 874 | 1249 |  |
|  | Factored Total Load |  | 384 | 606 | 637 | 910 | 966 | 1178 | 1387 | 1609 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 2.0/5.1 | 2.1/5.3 | 3.1/7.6 | 3.2/8.1 | 4.0/9.9 | 4.7/11.6 | 5.4/13.5 |
| 12 | Unfactored Load (LL) L/360 |  | 71 | 144 | 155 | 267 | 292 | 462 | 664 | 907 |
|  | Unfactored Load (TL) L/240 |  | 103 | 212 | 229 | 396 | 434 | 688 | 990 | 1354 |
|  | Factored Total Load |  | 322 | 508 | 534 | 764 | 811 | 1061 | 1245 | 1440 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.9/4.7 | 2.0/4.9 | 2.8/7.0 | 3.0/7.4 | 3.9/9.7 | 4.6/11.4 | 5.3/13.2 |
| 13 | Unfactored Load (LL) L/360 |  | 56 | 114 | 123 | 213 | 233 | 375 | 535 | 735 |
|  | Unfactored Load (TL) L/240 |  | 81 | 167 | 181 | 315 | 345 | 550 | 796 | 1095 |
|  | Factored Total Load |  | 274 | 433 | 455 | 650 | 690 | 939 | 1130 | 1304 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.7/4.3 | 1.8/4.5 | 2.6/6.4 | 2.7/6.8 | 3.7/9.3 | 4.5/11.2 | 5.2/12.9 |
| 14 | Unfactored Load (LL) L/360 |  | 45 | 92 | 99 | 172 | 189 | 301 | 437 | 602 |
|  | Unfactored Load (TL) L/240 |  | 65 | 134 | 145 | 254 | 279 | 446 | 649 | 896 |
|  | Factored Total Load |  | 236 | 373 | 392 | 560 | 595 | 809 | 1035 | 1191 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.6/4.0 | 1.7/4.2 | 2.4/6.0 | 2.5/6.4 | 3.5/8.6 | 4.4/11.1 | 5.1/12.7 |
| 15 | Unfactored Load (LL) L/360 |  | 37 | 75 | 81 | 141 | 155 | 248 | 361 | 499 |
|  | Unfactored Load (TL) L/240 |  | 52 | 109 | 118 | 208 | 228 | 367 | 535 | 742 |
|  | Factored Total Load |  | 205 | 324 | 341 | 487 | 517 | 704 | 904 | 1096 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.5/3.7 | 1.6/3.9 | 2.2/5.6 | 2.4/5.9 | 3.2/8.1 | 4.1/10.3 | 5.0/12.5 |
| 16 | Unfactored Load (LL) L/360 |  |  | 62 | 67 | 117 | 129 | 206 | 301 | 418 |
|  | Unfactored Load (TL) L/240 |  |  | 90 | 97 | 172 | 188 | 304 | 446 | 620 |
|  | Factored Total Load |  |  | 284 | 299 | 428 | 454 | 618 | 794 | 989 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.7 | 2.1/5.2 | 2.2/5.5 | 3.0/7.5 | 3.9/9.7 | 4.8/12.1 |
| 17 | Unfactored Load (LL) L/360 |  |  | 52 | 56 | 98 | 108 | 174 | 254 | 353 |
|  | Unfactored Load (TL) L/240 |  |  | 75 | 81 | 143 | 157 | 255 | 375 | 523 |
|  | Factored Total Load |  |  | 252 | 264 | 378 | 402 | 547 | 702 | 875 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.5 | 2.0/4.9 | 2.1/5.2 | 2.8/7.1 | 3.6/9.1 | 4.5/11.4 |
| 18 | Unfactored Load (LL) L/360 |  |  | 44 | 48 | 83 | 91 | 147 | 216 | 301 |
|  | Unfactored Load (TL) L/240 |  |  | 62 | 68 | 121 | 133 | 216 | 318 | 445 |
|  | Factored Total Load |  |  | 224 | 235 | 337 | 358 | 487 | 626 | 780 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.5 | 1.9/4.6 | 2.0/4.9 | 2.716.7 | 3.4/8.6 | 4.3/10.7 |
| 19 | Unfactored Load (LL) L/360 |  |  |  | 41 | 71 | 78 | 126 | 185 | 259 |
|  | Unfactored Load (TL) L/240 |  |  |  | 57 | 102 | 113 | 184 | 271 | 381 |
|  | Factored Total Load |  |  |  | 211 | 302 | 321 | 437 | 561 | 699 |
|  | Min. End / Int. Bearing (in) |  |  |  | 1.5/3.5 | 1.8/4.4 | 1.9/4.7 | 2.5/6.3 | 3.3/8.1 | 4.1/10.1 |
| 20 | Unfactored Load (LL) L/360 |  |  |  |  | 61 | 67 | 109 | 160 | 224 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 87 | 96 | 158 | 233 | 329 |
|  | Factored Total Load |  |  |  |  | 272 | 289 | 394 | 506 | 630 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.7/4.2 | 1.8/4.4 | 2.4/6.0 | 3.1/7.7 | 3.8/9.6 |
| 21 | Unfactored Load (LL) L/360 |  |  |  |  | 53 | 58 | 94 | 139 | 195 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 75 | 83 | 136 | 202 | 285 |
|  | Factored Total Load |  |  |  |  | 246 | 262 | 357 | 458 | 571 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.6/3.9 | 1.7/4.2 | 2.3/5.7 | 2.9/7.3 | 3.7/9.2 |
| 22 | Unfactored Load (LL) L/360 |  |  |  |  | 46 | 51 | 82 | 121 | 170 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 65 | 72 | 118 | 176 | 249 |
|  | Factored Total Load |  |  |  |  | 224 | 238 | 324 | 417 | 520 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.5/3.8 | 1.6/4.0 | 2.2/5.4 | 2.8/7.0 | 3.5/8.7 |
| 23 | Unfactored Load (LL) L/360 |  |  |  |  |  | 45 | 72 | 107 | 150 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  | 62 | 103 | 154 | 218 |
|  | Factored Total Load |  |  |  |  |  | 217 | 296 | 381 | 475 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  | 1.5/3.8 | 2.1/5.2 | 2.716.7 | 3.3/8.3 |
| 24 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 64 | 94 | 133 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 90 | 135 | 192 |
|  | Factored Total Load |  |  |  |  |  |  | 272 | 349 | 436 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 2.0/5.0 | 2.6/6.4 | 3.2/8.0 |
| 26 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 50 | 75 | 105 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 70 | 106 | 151 |
|  | Factored Total Load |  |  |  |  |  |  | 231 | 297 | 370 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.8/4.6 | 2.4/5.9 | 2.9/7.3 |
| 28 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 41 | 60 | 85 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 55 | 84 | 120 |
|  | Factored Total Load |  |  |  |  |  |  | 198 | 255 | 318 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.7/4.2 | 2.2/5.4 | 2.716.8 |
| 30 | Unfactored Load (LL) L/360 |  |  |  |  |  |  |  | 49 | 69 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  |  | 67 | 97 |
|  | Factored Total Load |  |  |  |  |  |  |  | 221 | 276 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  |  | 2.0/5.1 | 2.5/6.3 |

Verify adequacy of beam in uniform load tables prior to using values listed below.
$\mathbf{3 0 0 0 F}_{\mathrm{b}}-1.8 \mathrm{E} 1 \frac{1}{2}{ }^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL


* 4-ply beams should only be side-loaded when loads are applied to both sides of the member.

1. Nails to be located a minimum of $2^{\prime \prime}$ from the top and bottom of the member. Start all nails a minimum of $2 \frac{1}{2} 2^{\prime \prime}$ in from ends.
2. Bolts are to be material conforming to ASTM Standard A307. Bolt holes are to be the same diameter as the bolt, and located $2^{\prime \prime}$ from the top and bottom of the member. Washers should be used under head and nut. Start all bolts a minimum of $21 / 2^{\prime \prime}$ in from ends.
3. Values listed are for standard term loading.

E X A M P L E (All loads shown are total factored)
First, convert joist reactions to plf load on each side of the beam by taking the joist reaction (lbs.) divided by the joist spacing (ft.). $400 \mathrm{lbs} /(16 / 12)=300 \mathrm{plf}$ and $533 \mathrm{lbs} /(16 / 12)=400$ plf. Check factored resistance tables to verify that 3 plys can carry the total factored load of 700 plf. The maximum load applied to either outside member is 400 plf. Use 2 rows of $10 \mathrm{~d}\left(3^{\prime \prime}\right)$ common wire nails at $12^{\prime \prime}$ o.c. (good for 524 plf$)$.


## CONNECTION OF MULTIPLE PIECES FOR TOP-LOADED BEAMS

1.8E ( $1 \frac{1}{2}$ " wide pieces)

- Minimum of 2 rows of $10 \mathrm{~d}\left(3^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $5^{1} 2^{\prime \prime}$ through $117 / 8^{\prime \prime}$ beams
- Minimum of 3 rows of $10 \mathrm{~d}\left(3^{\prime \prime}\right)$ nails at $12^{\prime \prime} 0 . c$. for $14^{\prime \prime}$ through $18^{\prime \prime}$ beams



## EJ <br> Ulestifiser LVL <br> $3000 \mathrm{Fb}-1.8 \mathrm{E} 1^{3 / 4^{\prime \prime}}$ and $3^{11 / 2^{\prime \prime}}$ THICK

HEADERS AND BEAMS

## DESIGN PROPERTIES

$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E} 13 / \mathbf{4}^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91/2" | 111/2" | 117/8" | 14" | $16{ }^{\prime \prime}$ | 18" | 24" |
| Moment (ft.lbs.) | 4079 | 6827 | 10751 | 11299 | 16132 | 17126 | 23277 | 29855 | 37184 | 63568 |
| Shear (lbs.) | 3095 | 4080 | 5206 | 5347 | 6472 | 6683 | 7879 | 9005 | 10130 | 13507 |
| Moment of Inertia (in^4) | 24 | 56 | 115 | 125 | 222 | 244 | 400 | 597 | 851 | 2016 |
| Weight (lbs./lin.ft.) | 2.5 | 3.3 | 4.2 | 4.3 | 5.2 | 5.3 | 6.3 | 7.2 | 8.1 | 10.8 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. Lateral support of beam is required at bearing locations.
3. All $16^{\prime \prime}$ and greater beam depths are to be used in multiple member units only.
$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E} 3112^{\prime \prime}$ WEST FRASER ${ }^{\text {Tm }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91/2" | 111/2" | 117/8" | 14 " | 16" | 18" | 24" |
| Moment (ft.lbs.) | 8159 | 13654 | 21501 | 22597 | 32264 | 34252 | 46553 | 59709 | 74368 | 127136 |
| Shear (lbs.) | 6191 | 8161 | 10412 | 10693 | 12944 | 13367 | 15758 | 18010 | 20261 | 27014 |
| Moment of Inertia (in^4) | 49 | 111 | 231 | 250 | 444 | 488 | 800 | 1195 | 1701 | 4032 |
| Weight (lbs./lin.ft.) | 4.9 | 6.5 | 8.3 | 8.5 | 10.3 | 10.7 | 12.6 | 14.4 | 16.2 | 21.6 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. Lateral support of beam is required at bearing locations.
$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E} 13 / 4^{\prime \prime}$ AND $312^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL AVAILABLE SIZES

$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E}$ WEST FRASER ${ }^{\text {TM }}$ LVL SPECIFIED STRENGTHS (STANDARD TERM)
Modulus of Elasticity
Bending Stress
Shear (joist)
Compression Perpendicular to Grain (joist)
Compression Parallel to Grain

$$
\begin{aligned}
\mathrm{E} & =1.8 \times 10 \wedge 6 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{b}} & =5544 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{V}} & =536 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { perp })} & =1365 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { para })} & =3750 \mathrm{psi}
\end{aligned}
$$

1. $\mathrm{F}_{\mathrm{b}}$ based on $12^{\prime \prime}$ depths. For other depths, multiply by ( $\left.12 / \mathrm{d}\right)^{\wedge}(1 / 7.35)$.
2. $\mathrm{F}_{\mathrm{c}(\text { perp })}$ and E shall not be increased for duration of load.

## GENERAL NOTES

- Tables are for one-ply $13 / 4$ " beams. When properly connected, double the values for two-ply beams, triple for three. Minimum bearing lengths shown for one-ply will be the same for two-ply and three-ply. See page 25 for multiple-ply connection details.
- Resistances shown are the maximum factored and/or unfactored resistances, in pounds per lineal foot, that can be applied to the beam in addition to its own weight.
- Tables are based on uniform loads and the most restrictive of simple or continuous spans and dry-use conditions. Refer to West Fraser's sizing software for other loads or span configurations.
- Lateral support of beam compression edges is required at intervals of $24^{\prime \prime}$ o/c or closer.
- Lateral support of beams is required at bearing locations.
- West Fraser ${ }^{\text {rM }}$ LVL beams are made without camber; therefore, in addition to complying with the deflection limits of the applicable building code, other deflection considerations, such as long term deflection under sustained loads (including creep), must be evaluated.
- All $16^{\prime \prime}$ and deeper beams are to be used in multiple member units only.
- Unfactored total load resistance is limited to a deflection of L/240. Unfactored live load resistance is based on a deflection of L/360. Check local code requirements for other deflection criteria.
- For an unfactored live load deflection limit of L/480, multiply UNFACTORED LOAD L/360 resistance by 0.75 .
- Roof must have positive slope in order to prevent ponding.
- Spans of multiple spans must be at least $40 \%$ of adjacent span.
- Bearing lengths are based on 1365 psi specified strength for 1.8E Grade materials which cannot be increased for duration of load. Bearing length may need to be increased if support member's allowable bearing stress is less.
- Tables will accommodate beam slopes to a maximum of 2:12.


## INSTRUCTIONS FOR USE

1. Determine the factored total load and unfactored total and live load on the beam in pounds per lineal foot (plf).
2. Locate a span that meets or exceeds the required beam span, centre-to-centre of bearing.
3. Scan from left to right within the SPAN row until you find a cell where; (1) the UNFACTORED LOAD L/360 resistance meets or exceeds the unfactored live load, (2) the UNFACTORED LOAD L/240 resistance
meets or exceeds the unfactored total load and (3) the FACTORED TOTAL LOAD resistance meets or exceeds the factored total load. All three rows must be checked and satisfied. Where no unfactored resistances are shown, factored total load will control.
4. To size a member for a span not shown, use capacities for the next larger span shown.

FACTORED RESISTANCE TABLE (pounos perluneal foot)

## $3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E}$ West Fraser ${ }^{\text {T" }}$ LVL - FLOOR or ROOF (Standard Term)

| Span (ft) |  | 13/4" WIDTH |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Depth | 5-1/2" | 7-1/4" | 9-1/4" | 9-1/2" | 11-1/2" | 11-7/8" | $14 "$ | $16 "$ | 18" | 24" |
| 6 | Unfactored Load (LL) L/360 | 275 | 594 | 1137 | 1218 | 1967 | 2126 |  |  |  |  |
|  | Unfactored Load (TL) L/240 | 410 | 887 | 1701 |  |  |  |  |  |  |  |
|  | Factored Total Load | 904 | 1294 | 1743 | 1803 | 2313 | 2416 | 3044 | 3719 | 4494 | 7708 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 2.0/5.1 | 2.716.8 | 2.877.1 | 3.6/9.1 | 3.8/9.5 | 4.8/11.9 | 5.8/14.6 | 7.1/17.6 | 12.1/30.3 |
| 7 | Unfactored Load (LL) L/360 | 177 | 388 | 756 | 812 | 1339 | 1453 | 2181 |  |  |  |
|  | Unfactored Load (TL) L/240 | 263 | 578 | 1131 | 1214 |  |  |  |  |  |  |
|  | Factored Total Load | 664 | 1079 | 1440 | 1488 | 1889 | 1969 | 2450 | 2953 | 3516 | 5676 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 2.0/4.9 | 2.6/6.6 | 2.7/6.8 | 3.5/8.6 | 3.6/9.0 | 4.5/11.2 | 5.4/13.5 | 6.4/16.1 | 10.4/26.0 |
| 8 | Unfactored Load (LL) L/360 | 120 | 266 | 526 | 566 | 947 | 1030 | 1571 | 2181 | 2876 |  |
|  | Unfactored Load (TL) L/240 | 178 | 396 | 785 | 845 | 1415 | 1539 |  |  |  |  |
|  | Factored Total Load | 507 | 850 | 1227 | 1266 | 1596 | 1661 | 2049 | 2449 | 2886 | 4492 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.8/4.4 | 2.616.4 | 2.6/6.6 | 3.3/8.4 | 3.5/8.7 | 4.3/10.7 | 5.1/12.8 | 6.0/15.1 | 9.4/23.5 |
| 9 | Unfactored Load (LL) L/360 | 85 | 190 | 379 | 409 | 691 | 753 | 1163 | 1634 | 2181 |  |
|  | Unfactored Load (TL) L/240 | 126 | 282 | 565 | 609 | 1031 | 1125 | 1739 |  |  |  |
|  | Factored Total Load | 400 | 671 | 1058 | 1102 | 1382 | 1436 | 1761 | 2091 | 2448 | 3715 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.6/4.0 | 2.5/6.2 | 2.6/6.5 | 3.3/8.1 | 3.4/8.5 | 4.1/10.4 | 4.9/12.3 | 5.8/14.4 | 8.7/21.9 |
| 10 | Unfactored Load (LL) L/360 | 63 | 140 | 282 | 304 | 518 | 566 | 883 | 1251 | 1685 |  |
|  | Unfactored Load (TL) L/240 | 92 | 207 | 419 | 452 | 772 | 844 | 1318 |  |  |  |
|  | Factored Total Load | 324 | 543 | 856 | 900 | 1218 | 1265 | 1544 | 1824 | 2125 | 3167 |
|  | Min. End / Int. Bearing (in) | 1.5/3.5 | 1.5/3.6 | 2.2/5.6 | 2.4/5.9 | 3.2/8.0 | 3.3/8.3 | 4.0/10.1 | 4.8/11.9 | 5.6/13.9 | 8.3/20.7 |
| 11 | Unfactored Load (LL) L/360 |  | 106 | 215 | 232 | 398 | 435 | 684 | 976 | 1325 | 2679 |
|  | Unfactored Load (TL) L/240 |  | 156 | 318 | 344 | 592 | 647 | 1019 | 1457 |  |  |
|  | Factored Total Load |  | 448 | 707 | 743 | 1061 | 1127 | 1374 | 1618 | 1877 | 2760 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 2.0/5.1 | 2.1/5.3 | 3.1/7.6 | 3.2/8.1 | 4.0/9.9 | 4.7/11.6 | 5.4/13.5 | 7.9/19.9 |
| 12 | Unfactored Load (LL) L/360 |  | 83 | 168 | 181 | 312 | 341 | 539 | 775 | 1058 | 2181 |
|  | Unfactored Load (TL) L/240 |  | 121 | 247 | 267 | 462 | 506 | 803 | 1155 | 1580 |  |
|  | Factored Total Load |  | 376 | 593 | 623 | 891 | 946 | 1238 | 1453 | 1680 | 2445 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.9/4.7 | 2.014.9 | 2.817 .0 | 3.0/7.4 | 3.9/9.7 | 4.6/11.4 | 5.3/13.2 | 7.7119.2 |
| 13 | Unfactored Load (LL) L/360 |  | 65 | 133 | 144 | 248 | 272 | 432 | 624 | 857 | 1795 |
|  | Unfactored Load (TL) L/240 |  | 95 | 195 | 211 | 368 | 403 | 642 | 929 | 1277 |  |
|  | Factored Total Load |  | 320 | 505 | 531 | 758 | 805 | 1096 | 1319 | 1521 | 2194 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.7/4.3 | 1.8/4.5 | 2.6/6.4 | 2.7/6.8 | 3.719.3 | 4.5/11.2 | 5.2/12.9 | 7.5/18.7 |
| 14 | Unfactored Load (LL) L/360 |  | 53 | 107 | 116 | 201 | 220 | 351 | 510 | 703 | 1492 |
|  | Unfactored Load (TL) L/240 |  | 75 | 157 | 169 | 296 | 325 | 521 | 757 | 1046 |  |
|  | Factored Total Load |  | 275 | 435 | 457 | 653 | 694 | 944 | 1207 | 1389 | 1990 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.6/4.0 | 1.7/4.2 | 2.4/6.0 | 2.5/6.4 | 3.5/8.6 | 4.4/11.1 | 5.1/12.7 | 7.3/18.2 |
| 15 | Unfactored Load (LL) L/360 |  | 43 | 88 | 95 | 165 | 181 | 289 | 421 | 583 | 1251 |
|  | Unfactored Load (TL) L/240 |  | 61 | 127 | 138 | 242 | 266 | 428 | 624 | 866 |  |
|  | Factored Total Load |  | 239 | 378 | 397 | 568 | 604 | 821 | 1054 | 1278 | 1821 |
|  | Min. End / Int. Bearing (in) |  | 1.5/3.5 | 1.5/3.7 | 1.6/3.9 | 2.2/5.6 | 2.4/5.9 | 3.2/8.1 | 4.1/10.3 | 5.0/12.5 | 7.1/17.9 |
| 16 | Unfactored Load (LL) L/360 |  |  | 73 | 78 | 137 | 150 | 241 | 351 | 488 | 1058 |
|  | Unfactored Load (TL) L/240 |  |  | 105 | 113 | 200 | 220 | 355 | 520 | 724 | 1577 |
|  | Factored Total Load |  |  | 332 | 349 | 499 | 530 | 721 | 926 | 1154 | 1678 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.7 | 2.1/5.2 | 2.2/5.5 | 3.017.5 | 3.9/9.7 | 4.8/12.1 | 7.0117.6 |
| 17 | Unfactored Load (LL) L/360 |  |  | 61 | 66 | 115 | 126 | 203 | 296 | 412 | 902 |
|  | Unfactored Load (TL) L/240 |  |  | 87 | 94 | 167 | 184 | 298 | 437 | 610 | 1343 |
|  | Factored Total Load |  |  | 293 | 308 | 441 | 469 | 638 | 819 | 1021 | 1555 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.5 | 2.0/4.9 | 2.1/5.2 | 2.8/7.1 | 3.6/9.1 | 4.5/11.4 | 6.9/17.3 |
| 18 | Unfactored Load (LL) L/360 |  |  | 51 | 56 | 97 | 107 | 172 | 252 | 351 | 775 |
|  | Unfactored Load (TL) L/240 |  |  | 73 | 79 | 141 | 155 | 252 | 371 | 519 | 1152 |
|  | Factored Total Load |  |  | 261 | 275 | 393 | 418 | 568 | 730 | 910 | 1449 |
|  | Min. End / Int. Bearing (in) |  |  | 1.5/3.5 | 1.5/3.5 | 1.9/4.6 | 2.0/4.9 | 2.716 .7 | 3.4/8.6 | 4.3/10.7 | 6.8/17.1 |
| 19 | Unfactored Load (LL) L/360 |  |  |  | 47 | 83 | 91 | 147 | 216 | 302 | 670 |
|  | Unfactored Load (TL) L/240 |  |  |  | 67 | 119 | 131 | 214 | 317 | 445 | 994 |
|  | Factored Total Load |  |  |  | 246 | 352 | 374 | 510 | 654 | 816 | 1357 |
|  | Min. End / Int. Bearing (in) |  |  |  | 1.5/3.5 | 1.7/4.4 | 1.9/4.6 | 2.5/6.3 | 3.3/8.1 | 4.1/10.1 | 6.7/16.9 |
| 20 | Unfactored Load (LL) L/360 |  |  |  |  | 71 | 78 | 127 | 186 | 261 | 583 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 102 | 112 | 184 | 272 | 383 | 863 |
|  | Factored Total Load |  |  |  |  | 317 | 337 | 459 | 590 | 736 | 1261 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.7/4.1 | 1.8/4.4 | 2.4/6.0 | 3.1/7.7 | 3.9/9.6 | 6.6/16.5 |
| 21 | Unfactored Load (LL) L/360 |  |  |  |  | 62 | 68 | 110 | 162 | 227 | 510 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 88 | 97 | 159 | 236 | 333 | 753 |
|  | Factored Total Load |  |  |  |  | 287 | 305 | 416 | 534 | 666 | 1142 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.6/3.9 | 1.7/4.2 | 2.3/5.7 | 2.9/7.3 | 3.7/9.1 | 6.3/15.7 |
| 22 | Unfactored Load (LL) L/360 |  |  |  |  | 54 | 59 | 96 | 142 | 199 | 448 |
|  | Unfactored Load (TL) L/240 |  |  |  |  | 76 | 84 | 138 | 205 | 290 | 661 |
|  | Factored Total Load |  |  |  |  | 261 | 278 | 378 | 486 | 607 | 1040 |
|  | Min. End / Int. Bearing (in) |  |  |  |  | 1.5/3.8 | 1.6/4.0 | 2.2/5.4 | 2.817.0 | 3.5/8.7 | 6.0/15.0 |
| 23 | Unfactored Load (LL) L/360 |  |  |  |  |  | 52 | 84 | 124 | 175 | 396 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  | 73 | 120 | 180 | 254 | 583 |
|  | Factored Total Load |  |  |  |  |  | 254 | 346 | 444 | 554 | 951 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  | 1.5/3.8 | 2.1/5.2 | 2.716.7 | 3.3/8.3 | 5.7/14.3 |
| 24 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 74 | 110 | 155 | 351 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 105 | 158 | 224 | 516 |
|  | Factored Total Load |  |  |  |  |  |  | 317 | 407 | 508 | 872 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 2.0/5.0 | 2.6/6.4 | 3.2/8.0 | 5.5/13.7 |
| 26 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 59 | 87 | 123 | 280 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 82 | 123 | 176 | 410 |
|  | Factored Total Load |  |  |  |  |  |  | 269 | 346 | 432 | 741 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.8/4.6 | 2.4/5.9 | 2.9/7.3 | 5.0/12.6 |
| 28 | Unfactored Load (LL) L/360 |  |  |  |  |  |  | 47 | 70 | 99 | 227 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  | 65 | 98 | 140 | 330 |
|  | Factored Total Load |  |  |  |  |  |  | 231 | 297 | 371 | 638 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  | 1.7/4.2 | 2.2/5.4 | 2.7/6.8 | 4.7/11.7 |
| 30 | Unfactored Load (LL) L/360 |  |  |  |  |  |  |  | 57 | 81 | 186 |
|  | Unfactored Load (TL) L/240 |  |  |  |  |  |  |  | 79 | 113 | 269 |
|  | Factored Total Load |  |  |  |  |  |  |  | 258 | 322 | 554 |
|  | Min. End / Int. Bearing (in) |  |  |  |  |  |  |  | 2.0/5.1 | 2.5/6.3 | 4.3/10.9 |

[^3]LVL USER'S GUIDE

Verify adequacy of beam in uniform load tables prior to using values listed below.
$3000 \mathrm{~F}_{\mathrm{b}}-1.8 \mathrm{E}$ 13/4" WEST FRASER ${ }^{\text {TM }}$ LVL


* 4-ply beams should only be side-loaded when loads are applied to both sides of the member.

1. Nails to be located a minimum of $2^{\prime \prime}$ from the top and bottom of the member. Start all nails a minimum of $21 / 2^{\prime \prime}$ in from ends.
2. Bolts are to be material conforming to ASTM Standard A307. Bolt holes are to be the same diameter as the bolt, and located $2^{\prime \prime}$ from the top and bottom of the member. Washers should be used under head and nut. Start all bolts a minimum of $2 \frac{1}{2 \prime \prime}$ " in from ends.
3. Values listed are for standard term loading.

E XAMPLE (All loads shown are total factored)
First, convert joist reactions to plf load on each side of the beam by taking the joist reaction (lbs.) divided by the joist spacing (ft.). $400 \mathrm{lbs} /(16 / 12)=300 \mathrm{plf}$ and $533 \mathrm{lbs} /(16 / 12)=400$ plf. Check factored resistance tables to verify that 3 plys can carry the total factored load of 700 plf. The maximum load applied to either outside member is 400 plf. Use 2 rows of $16 \mathrm{~d}\left(31 / 2^{\prime \prime}\right)$ common wire nails at $12^{\prime \prime}$ o.c. (good for 620 plf ).


CONNECTION OF MULTIPLE PIECES FOR TOP-LOADED BEAMS
1.8E ( $13 / 4^{\prime \prime}$ wide pieces)

- Minimum of 2 rows of $16 d\left(31 / 2^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $5 \frac{1}{2} 2^{\prime \prime}$ through $117 / 8^{\prime \prime}$ beams
- Minimum of 3 rows of $16 \mathrm{~d}\left(31 / 2^{\prime \prime}\right)$ nails at $12^{\prime \prime}$ o.c. for $14^{\prime \prime}$ through $24^{\prime \prime}$ beams



## ALLOWABLE FACTORED AXIAL LOADS (LBS)

| Column Length ( ft ) | $31121 \times 3112{ }^{\prime \prime}$ | $31 / 22^{\prime \prime} \times 43 / 8$ | $31122^{\prime \prime} \times 51 / 2^{\prime \prime}$ | $31 / 2{ }^{\prime \prime} \times 71 / 4^{\prime \prime}$ | $31 / 2{ }^{\prime \prime} \times 85 /{ }^{\text {" }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 29528 | 35645 | 42891 | 52930 | 59895 |
| 4 | 26678 | 32173 | 38688 | 47748 | 54072 |
| 5 | 23161 | 27939 | 33629 | 41606 | 47232 |
| 6 | 19503 | 23568 | 28442 | 35350 | 40283 |
| 7 | 16124 | 19541 | 23671 | 29592 | 33872 |
| 8 | 13219 | 16076 | 19558 | 24602 | 28289 |
| 9 | 10814 | 13200 | 16129 | 20413 | 23576 |
| 10 | 8856 | 10849 | 13312 | 16947 | 19653 |
| 12 | 5993 | 7390 | 9137 | 11753 | 13729 |
| 14 | 4132 | 5120 | 6367 | 8256 | 9701 |

1. Loads are based on the allowable crushing of the LVL material, i.e., steel bearing connections.

## COLUMN DETAILS

## BEAM ON COLUMN CAP



COLUMN BASE


ELEVATED COLUMN BASE

beam on column


ALLOWABLE FACTORED AXIAL LOADS (LBS) - WOOD PLATE BEARING CONNECTIONS

| Column Length ( ft ) | $31 / 22^{\prime \prime} \times 31 / 2^{\prime \prime}$ | $31 / 2 \mathrm{~L} \times 43 / 8{ }^{\text {" }}$ | $311 / 2^{\prime \prime} \times 5112{ }^{\prime \prime}$ | $31 / 22^{\prime \prime} \times 71 / 4{ }^{\prime \prime}$ | $31 / 22^{\prime \prime} \times 85 / 8^{\prime \prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 3-9 | 7526 | 9408 | 11827 | 15590 | 18547 |
| 10 | 7526 | 9408 | 11827 | 15590 | 18547 |
| 12 | 5993 | 7390 | 9137 | 11753 | 13729 |
| 14 | 4132 | 5120 | 6367 | 8256 | 9701 |

1. Loads are based on the allowable crushing of a wood plate (SPF, any grade), $F_{C p}=768$ psi.

## GENERAL NOTES

- Tables apply to solid, one-piece members only.
- Tables assumes that columns are unbraced, except at column ends.
- Column members to be used in dry service conditions only.
- Column length is the distance between the centers of restraining members.
- Tables include an eccentricity equal to $1 / 6$ of the larger column dimension (thickness or width).
- Loads are based on simple axial loaded columns. For side loads or other combined bending and axial loads, see the provisions of CSA Standard 086-09.
- Factored resistances are based on standard term loading.


# Es <br> Hest froser LVL 2750Fb - 1.7E LVL 

## sist froser-LVL

## 2750 Fb - $1.7 \mathrm{E} 1^{3 / 4^{\prime \prime}}$ and $3^{1 / 22^{\prime \prime}}$ THICK

## HEADERS, BEAMS AND COLUMNS

## DESIGN PROPERTIES

$2750 \mathrm{~F}_{\mathrm{b}}-1.7 \mathrm{E} 13 / 4^{\prime \prime}{ }^{\prime \prime}$ WEST FRASER ${ }^{\text {Tm }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91⁄2" | 111⁄2" | 117/8" | 14" | $16 "$ | 18" | 24" |
| Moment (ft.lbs.) | 3667 | 6180 | 9791 | 10297 | 14772 | 15695 | 21419 | 27564 | 34432 | 59287 |
| Shear (lbs.) | 3095 | 4080 | 5206 | 5347 | 6472 | 6683 | 7879 | 9005 | 10130 | 13507 |
| Moment of Inertia (in^4) | 24 | 56 | 115 | 125 | 222 | 244 | 400 | 597 | 851 | 2016 |
| Weight (lbs./lin.ft.) | 2.5 | 3.3 | 4.2 | 4.3 | 5.2 | 5.3 | 6.3 | 7.2 | 8.1 | 10.8 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. All $16^{\prime \prime}$ and greater beam depths are to be used in multiple member units only.
. Lateral support of beam is required at bearing locations.
$2750 \mathrm{~F}_{\mathrm{b}}-1.7 \mathrm{E}$ ½" WEST FRASER ${ }^{\text {TM }}$ LVL FACTORED RESISTANCES (STANDARD TERM)

| Design Property | Depth |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 51/2" | 71/4" | 91/4" | 91/2" | 111/2" | 117/8" | 14" | 16 " | 18" | 24" |
| Moment (ft.lbs.) | 7335 | 12360 | 19582 | 20594 | 29544 | 31390 | 42838 | 55128 | 68864 | 118573 |
| Shear (lbs.) | 6191 | 8161 | 10412 | 10693 | 12944 | 13367 | 15758 | 18010 | 20261 | 27014 |
| Moment of Inertia (in^4) | 49 | 111 | 231 | 250 | 444 | 488 | 800 | 1195 | 1701 | 4032 |
| Weight (lbs./lin.ft.) | 4.9 | 6.5 | 8.3 | 8.5 | 10.3 | 10.7 | 12.6 | 14.4 | 16.2 | 21.6 |

1. Lateral support of beam compression edge is required at intervals of $24^{\prime \prime} \mathrm{o} / \mathrm{c}$ or closer.
2. Lateral support of beam is required at bearing locations.
$2750 \mathrm{~F}_{\mathrm{b}}-1.7 \mathrm{E} 13 / 4^{\prime \prime}$ AND $31 / 2^{\prime \prime}$ WEST FRASER ${ }^{\text {TM }}$ LVL AVAILABLE SIZES


## $2750 \mathrm{~F}_{\mathrm{b}}-1.7 \mathrm{E}$ WEST FRASER ${ }^{T M}$ LVL SPECIFIED STRENGTHS (STANDARD TERM)

[^4]\[

$$
\begin{aligned}
\mathrm{E} & =1.7 \times 10 \wedge 6 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{b}} & =5082 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{V}} & =536 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { perp })} & =1363 \mathrm{psi} \\
\mathrm{~F}_{\mathrm{c}(\text { para })} & =3756 \mathrm{psi}
\end{aligned}
$$
\]

# E $\underbrace{}_{\text {Ullest finser LVL }}$ <br> Miscellaneous Details, Software and Warranty Information 



B1 BEARING AT WALL


BEARING AT CONCRETE WALL


B2 BEARING FOR DOOR OR WINDOW HEADER


B5 BEARING AT WOOD OR STEEL COLUMN
Verify column capacity and bearing length.


B3 BEAM-TO-BEAM CONNECTION


## BEARING LENGTH IS EXTREMELY CRITICAL AND MUST BE CONSIDERED FOR EACH APPLICATION.

Multiple pieces of West Fraser ${ }^{\text {TM }}$ LVL can be nailed or bolted together to form a header or beam of the required size, up to a maximum width of 5 inches for $11 / 4^{\prime \prime}$ wide pieces and 7 inches for $13 / 4^{\prime \prime}$ wide pieces. See pages 9,15 , 21 and 25 for details.

## ALLOWABLE HOLES



## GENERAL NOTES

- The Allowed Hole Zone in this chart is suitable for Uniformly loaded beams using maximum loads for any tables listed. For other load conditions or hole configurations, please contact West Fraser.
- If more than one hole is to be cut in the beam, the length of the uncut beam between holes must be a minimum of twice the diameter of the largest hole.
- Rectangular holes are not allowed.
- Holes in cantilevers require additional analysis.
- For beam depths of $31 / 2^{\prime \prime}, 51 / 2^{\prime \prime}$ and $71_{4}^{\prime \prime}$, the maximum hole diameter is $3 / 4^{\prime \prime}, 11 / 8^{\prime \prime}$ and $11 / 2^{\prime \prime}$ respectively. For deeper beams, the maximum hole diameter is $2^{\prime \prime}$. The maximum number of holes for each span is limited to 3.


Do not cut, notch or drill holes in West Fraser ${ }^{\text {TM }}$ LVL except as indicated in illustration for allowable holes


Do not overhang seat cuts on West Fraser ${ }^{\text {TM }}$ LVL beams from inside face of support member


Do not notch underside of beam at bearing location


## MINIMUM NAIL SPACING

| Connector | Nailing Parallel to Glue Line | Nailing Perpendicular to Glue Line |
| :--- | :---: | :---: |
| 8d Box | $3^{\prime \prime}$ | $2^{\prime \prime}$ |
| 8d Common | $3^{\prime \prime}$ | $2^{\prime \prime}$ |
| 10d and 12d Box | $4^{\prime \prime}$ | $2^{\prime \prime}$ |
| 10d and 12d Common | $4^{\prime \prime}$ | $3^{\prime \prime}$ |
| 16d Common | $8^{\prime \prime}$ | $3^{\prime \prime}$ |

* Not allowed on product thickness less than $11 / 2^{\prime \prime}$



## OUR WEATHER RESISTANT COATING



Photo shows example of the beading that occurs because of our coating process.

One of the inherent problems with LVL is its inability to resist the effects of moisture. West Fraser addresses this problem by coating all our LVL beams and headers with a protective sealer. This sealer gives our LVL superior resistance to warping, cupping, and swelling compared to other unprotected competitive products. While this coating is not intended to provide long-term protection, it does improve protection against the moisture associated with the construction process.

## OUR SOFTWARE

West Fraser provides its LVL customers with quality design software. Using the latest technology it's fast and reliable, providing you with an easy to understand output. Our software will enhance your in-house design capabilities and productivity.


## LIMITED LIFETIME WARRANTY

(*to non-consumer buyers)

Sundre Forest Products Inc. warrants that its WEST FRASER ${ }^{\text {TM }}$ LVL is free from defects in materials and workmanship, and, when correctly installed, will perform in accordance with Sundre Forest Products Inc.'s published specifications for the lifetime of the building.

West Fraser ${ }^{\text {TM }}$ LVL used anywhere else except as shown in our published specifications is not covered in this warranty.
*A non-consumer is a person or entity who purchases a product for purposes of resale or to incorporate into another product which will be resold.

## LIMITATIONS

Sundre Forest Products Inc. must be given a reasonable opportunity to inspect its WEST FRASERTM LVL before it will honor any claims under the above warranty.
If, after inspection, Sundre Forest Products Inc. determines that a product failure exists covered by the above warranty, Sundre Forest Products Inc. will pay to the owner of the structure an amount equal to the reasonable cost of labor and materials required to remove and replace or repair the defective product. The product must be protected from exposure to moisture from whatever source in accordance with provisions of the applicable building standards. Failure to protect the product from moisture, except for incidental exposure during construction, may cause the product to fail to perform as warranted and will void this limited lifetime warranty. Exposure to standing water and accumulations of snow and ice without reasonably prompt removal thereof will void this limited lifetime warranty.

## DISCLAIMER

Except for the express warranty and remedy set out above, Sundre Forest Products Inc. disclaims all other warranties and guaranties, express or implied, including implied warranties of merchantability or fitness for a particular purpose. No other warranty or guaranty will be made by or on behalf of the manufacturer or the seller or by operation of law with respect to the product or its installation, storage, handling, maintenance, use, replacement or repair. Neither Sundre Forest Products Inc. nor the seller shall be liable by virtue of any warranty or guaranty, or otherwise, for any special, incidental or consequential loss or damage resulting from the use of the product. Sundre Forest Products Inc. makes no warranty or guaranty with respect to installation of the product by the builder or the builder's contractor or any other installer.


[^0]:    Modulus of Elasticity
    Bending Stress
    Shear (joist)
    Compression Perpendicular to Grain (joist)
    Compression Parallel to Grain

[^1]:    * All 16 ", 18 " and 24 " beam depths are to be used in multiple member units only.

[^2]:    Modulus of Elasticity
    Bending Stress
    Shear (joist)
    Compression Perpendicular to Grain (joist)
    Compression Parallel to Grain

    1. Fb based on $12^{\prime \prime}$ depths. For other depths, multiply by $(12 / d) \wedge(1 / 7.35)$.
    2. Fc (perp) and E shall not be increased for duration of load.
[^3]:    * All $16^{\prime \prime}, 18^{\prime \prime}$ and 24 " beam depths are to be used in multiple member units only.

[^4]:    Modulus of Elasticity
    Bending Stress
    Shear (joist)
    Compression Perpendicular to Grain (joist)
    Compression Parallel to Grain

